



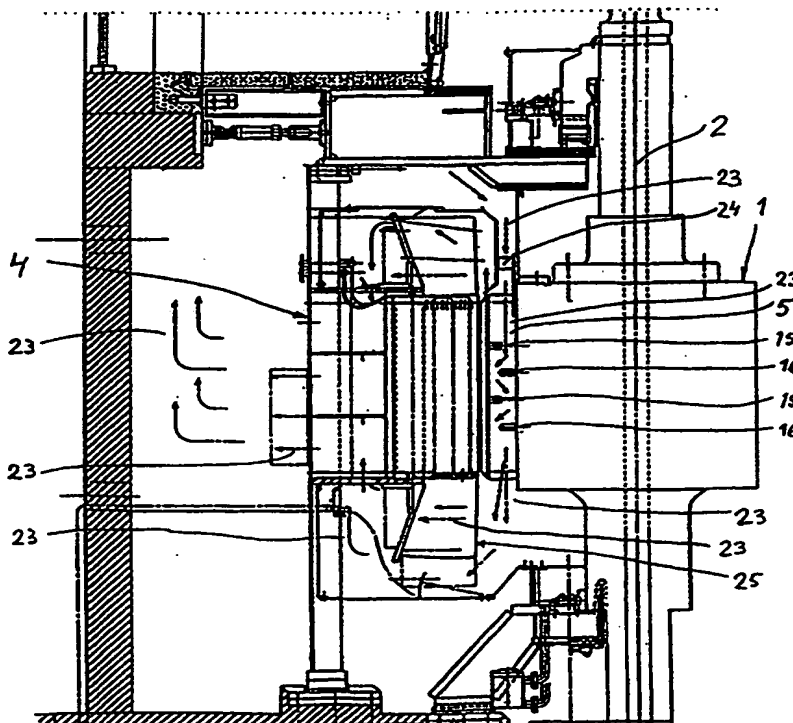
## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification <sup>6</sup> : <b>H02K 3/52</b>		A1	(11) International Publication Number: <b>WO 98/34328</b>
			(43) International Publication Date: 6 August 1998 (06.08.98)
(21) International Application Number: PCT/SE98/00164		(81) Designated States: AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, CZ (Utility model), DE, DE (Utility model), DK, DK (Utility model), EE, ES, FI, FI (Utility model), GB, GE, GH, GM, GW, HU, ID, IL, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).	
(22) International Filing Date: 2 February 1998 (02.02.98)			
(30) Priority Data: 9700352-9      3 February 1997 (03.02.97)      SE 9704423-4      28 November 1997 (28.11.97)      SE			
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(54) Title: ROTATING ELECTRIC MACHINE WITH COIL SUPPORTS

## (57) Abstract

The invention relates to a rotating electric machine comprising a stator (4) provided with windings drawn through slots in the stator, and a rotor (1) having a central axis (2) and poles (5, 6) in the form of pole pieces (8, 9) provided with windings and forming solenoids, pole gaps (13) being arranged between the poles. The machine also comprises coil supports (15, 16) in said pole gaps in order to support the solenoid windings (10, 11). It is characterized in that the coil supports (15, 16) are arranged in pairs and that each coil support (15, 16) is shaped so that it supports only a part of the solenoid windings (10, 11) of the two adjacent poles (5, 6).



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ROTATING ELECTRIC MACHINE WITH COIL SUPPORTS

The present invention relates to a rotating electric machine as described in the preamble to claim 1.

5

Examples of rotating electric machines are synchronous machines, normal asynchronous machines as well as double-fed machines, alternating current machines, applications in asynchronous static current converter cascades, outerpole machines and synchronous flux machines.

10

The machine according to the invention is intended in the first place as a generator in a power station for generating electric power.

15

In the present application the terms "radial", "axial", "tangential" and "peripheral" constitute indications of direction defined in relation to the rotor of the machine unless expressly stated otherwise.

20

For vertical rotating electric machines with salient poles, known as Salient Pole Machines, coil supports are conventionally used between the different poles. The reason for this is that the rotor poles comprise pole pieces provided with a winding so that solenoids (magnet coils) are formed. Since the pole has a certain width, the long sides of the coil will not be situated in an axial plane running through the centre of the rotor, i.e. an axial plane through the long sides of the coil will be displaced parallel to an axial plane through the radial centre line of the corresponding pole. Part of the centrifugal force arising when the rotor rotates will therefore influence the long sides with a tangential force in the direction of the periphery. This force will endeavour to press the metal in the coil winding away from contact with the pole piece. The long sides of the coil thus run the risk of being bent out and, in the worst case, coming into contact with each other,

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30

35

which may give rise to powerful short circuits which in turn cause disturbing magnetic imbalances.

5 In order to prevent short circuits of the type described above, therefore, special coil supports are fitted in the pole gap, i.e. the gap or space between two adjacent poles, when deemed necessary. The task of these coil supports is thus to keep the coil windings in place. Coil supports are especially common in coils in high-speed machines.

10 Conventional coil supports usually consist of one or more whole-block supports, i.e. solid, substantially V-shaped supports, arranged at a suitable axial distance from each other in each pole gap. Since it is desirable for the coil support  
15 to support the entire solenoid winding, each coil support will substantially block the entire area between two adjacent poles, i.e. the pole gap. The small space between two rotor poles which is not blocked by the coil support is used for ventilation so that cooling air can flow axially to cool  
20 the poles and later also the stator, depending on the type of rotating machine and the type of ventilation principle utilized. The spaces referred to are essentially the small space available near the air gap, between the rotor poles and the stator, and the equally limited space between the  
25 rotor windings and the rotor itself.

The types of ventilation which are relevant are the so called Midi-concept, axial ventilation and radial ventilation. In the Midi-concept the rotor body is used as a fan  
30 and the air passes axially through the pole gap from one side of the machine. In the case of axial ventilation axial fans are mounted on the rotor, usually two fans, one on the upper and one on the lower side. The air effects cooling of the poles and is transported axially to radial openings in  
35 the stator where it also has a cooling effect. In the absence of radial openings in the stator, however, the alternative using two axial fans is not possible. One-way axial

ventilation or radial ventilation (air flowing radially through the rotor) can however manage the ventilation without radial openings in the stator core. However, radial ventilation is not possible with small rotor diameters.

5

It is obvious that the cooling air, or possibly some other type of gas used for cooling, able to pass the coil supports is in many cases insufficient to achieve satisfactory cooling of the machine.

10

The flow of cooling air permitted to pass through the pole gap is also limited by the maximum rise in temperature permissible for the air and also by the air speed having to be restricted. The latter is because, when the air is conducted through the pole gaps, it is accelerated to a speed  
15 approaching the peripheral speed of the rotor. This results in an increase in the kinetic energy of the air which is entirely lost, however, when the air leaves the machine. A retarding moment is thus caused, and consequently a power  
20 loss, which is directly reflected in the efficiency of the machine. Since these ventilation losses are directly proportional to the air flow, it is therefore desirable to have as little air resistance as possible.

25

According to a known device, in which an attempt is made to solve the problem of insufficient ventilation, the coil supports have been provided with apertures in order to increase the available area for the flow of cooling air. Unfortunately, these coil supports in many cases still fail  
30 to provide satisfactory ventilation. Furthermore, the coil supports force the air away from the coils which results in at least some of the air flow instead flowing closer to the stator and thus passing too far away from the coils to be of any use.

35

From the document US 3 740 600 is previously known a coil support or brace which supports only part of the coil wind-

ings, namely those windings which are closest to the rotor piece. The purpose of the brace is to prevent separation of the coils from the poles by the tangential component of centrifugal force acting on the coils. The reason that the  
5 brace is designed to support only the innermost windings is that these windings, in the disclosed configuration of the poles, are particularly subjected said forces. Similar devices are also known from US 5 036 238, GB-A-2 022 327 and DE-A-25 20 511.

10 Through US 5 036 165 is known a conductor, in which the insulation is provided with an inner and an outer layer of semiconducting pyrolyzed glass fibre. It is also known to provide conductors in a dynamo-electric machine with such an  
15 insulation, as described in US 5 066 881 for instance, where a semiconducting pyrolyzed glass fibre layer is in contact with the two parallel bars forming the conductor, and the insulation in the stator slots is surrounded by an outer layer of semiconducting pyrolyzed glass fibre. The pyrolyzed  
20 glass fibre material is described as suitable since it retains its resistivity even after the impregnation treatment.

25 The object of the present invention is to provide a rotating electric machine designed to eliminate the above-mentioned problems and whereby satisfactory ventilation is obtained in an efficient and simple manner.

30 This object is achieved by a machine of the type described in the preamble to claim 1 having the special features defined in the characterizing part of the claim.

35 Accordingly, the coil supports are arranged in pairs, and each coil support in a pair is shaped so that it supports only a part of the solenoid windings of the two adjacent poles. To continue, two coil supports in a pair are arranged

axially and radially displaced in relation to each other to allow a cooling gas to flow between the coil supports.

Through this arrangement the advantage is gained that the area of the flow path for the air through the pole gaps is increased and the air resistance is decreased. A larger amount of air (or other gas) can thus pass at the same flow rate, and a higher degree of cooling is obtained. Alternatively, the same amount of air may be allowed to pass at a reduced rate, whereby said power losses are reduced and the efficiency of the machine increases. This in turn offers the advantage of being able to use only one fan instead of two, as is normal with axial ventilation. Satisfactory ventilation of the coil-end package beneath the stator is also made possible with this single fan. As compared to known devices for supporting only part of the windings, the present invention has the considerable advantage that all of the windings will be supported, thus resulting in a more reliable and altogether safer machine.

Another advantage is that, if radial ventilation (air flowing radially through the rotor) is not possible, particularly in rotors with small diameters, the present invention enables one-way axial ventilation through the entire pole gap to the lower side of the stator in combination with coil supports.

The coil supports characterized in claim 1 also have the advantage that they can be used both in rotating electric machines of conventional type and in high-voltage machines using cable, i.e. high-voltage insulating electric conductors, as stator winding. Particularly pronounced advantages are achieved when the machine according to the invention is provided with stator windings composed of high-voltage cable. The high-voltage cable lies in slots in the stator which are extra deep and vertically high, and efficient ventilation is thus particularly difficult to achieve, as well as the need for it being greater.

Consequently, in the rotating electric machine according to the invention, the windings are preferably composed of cables having solid, extruded insulation, of a type now used  
5 for power distribution, such as XLPE-cables or cables with EPR-insulation. Such a cable comprises an inner conductor composed of one or more strand parts, an inner semiconducting layer surrounding the conductor, a solid insulating layer surrounding this and an outer semiconducting layer  
10 surrounding the insulating layer. Such cables are flexible, which is an important property in this context since the technology for the device according to the invention is based primarily on winding systems in which the winding is formed from cable which is bent during assembly. The flexibility  
15 of a XLPE-cable normally corresponds to a radius of curvature of approximately 20 cm for a cable with a diameter of 30 mm, and a radius of curvature of approximately 65 cm for a cable with a diameter of 80 mm. In the present application the term "flexible" is used to indicate that the  
20 winding is flexible down to a radius of curvature in the order of four times the cable diameter, preferably eight to twelve times the cable diameter.

The winding should be constructed to retain its properties  
25 even when it is bent and when it is subjected to thermal stress during operation. It is vital that the layers retain their adhesion to each other in this context. The material properties of the layers are decisive here, particularly their elasticity and relative coefficients of thermal expansion.  
30 In a XLPE-cable, for instance, the insulating layer consists of cross-linked, low-density polyethylene, and the semiconducting layers consist of polyethylene with soot and metal particles mixed in. Changes in volume as a result of temperature fluctuations are completely absorbed as changes  
35 in radius in the cable and, thanks to the comparatively slight difference between the coefficients of thermal expansion in the layers in relation to the elasticity of these



materials, the radial expansion can take place without the adhesion between the layers being lost.

The material combinations stated above should be considered only as examples. Other combinations fulfilling the conditions specified and also the condition of being semiconducting, i.e. having resistivity within the range of  $10^{-1}$ - $10^6$  ohm-cm, e.g. 1-500 ohm-cm, or 10-200 ohm-cm, naturally also fall within the scope of the invention.

The insulating layer may consist, for example, of a solid thermoplastic material such as low-density polyethylene (LDPE), high-density polyethylene (HDPE), polypropylene (PP), polybutylene (PB), polymethyl pentene ("TPX"), cross-linked materials such as cross-linked polyethylene (XLPE), or rubber such as ethylene propylene rubber (EPR) or silicon rubber.

The inner and outer semiconducting layers may be of the same basic material but with particles of conducting material such as soot or metal powder mixed in.

The mechanical properties of these materials, particularly their coefficients of thermal expansion, are affected relatively little by whether soot or metal powder is mixed in or not - at least in the proportions required to achieve the conductivity necessary according to the invention. The insulating layer and the semiconducting layers thus have substantially the same coefficients of thermal expansion.

Ethylene-vinyl-acetate copolymers/nitrile rubber (EVA/NBR), butyl graft polyethylene, ethylene-butyl-acrylate copolymers (EBA) and ethylene-ethyl-acrylate copolymers (EEA) may also constitute suitable polymers for the semiconducting layers.

Even when different types of material are used as base in the various layers, it is desirable for their coefficients

of thermal expansion to be substantially the same. This is the case with the combination of the materials listed above.

5 The materials listed above have relatively good elasticity, with an E-modulus of  $E < 500$  MPa, preferably  $< 200$  MPa. The elasticity is sufficient for any minor differences between the coefficients of thermal expansion for the materials in the layers to be absorbed in the radial direction of the elasticity so that no cracks appear, or any other damage,  
10 and so that the layers are not released from each other. The material in the layers is elastic, and the adhesion between the layers is at least of the same magnitude as in the weakest of the materials.

15 The conductivity of the two semiconducting layers is sufficient to substantially equalize the potential along each layer. The conductivity of the outer semiconducting layer is sufficiently high to enclose the electrical field within the cable, but sufficiently low not to give rise to significant  
20 losses due to currents induced in the longitudinal direction of the layer.

Thus, each of the two semiconducting layers essentially constitutes one equipotential surface, and these layers will  
25 substantially enclose the electrical field between them.

There is, of course, nothing to prevent one or more additional semiconducting layers being arranged in the insulating layer.  
30

According to a particularly advantageous feature the stator windings are composed of high-voltage cable.

35 An additional characteristic is that the high-voltage cable has a diameter within the interval 20-250 mm and a conductor area within the interval 80-3000 mm<sup>2</sup>.

Further characteristics and advantages of the present invention are revealed in the remaining sub-claims.

According to another characteristic, each of the two coil supports in a pair covers substantially half the area occupied by the corresponding pole gap in the radial direction. The advantage is thus gained that the remainder of the pole-gap area, i.e. as much as the remaining 50%, is available for the air flow.

Alternatively, one of the two coil supports in a pair is arranged to support substantially half of the windings of the two adjacent poles and the other of the two coil supports is arranged to support substantially the other half of said windings.

According to yet another alternative, one of the two coil supports in a pair is arranged to support substantially half of the windings of the two adjacent poles and the other of the two coil supports is arranged to support the other half of said windings and an additional small number of windings in order to secure an overlap of supported windings. Through this alternative is achieved a particularly safe device due to the overlap of supported windings.

Finally, according to a particularly advantageous feature, the two coil supports in a pair are displaced axially by such a distance that the area in the axial direction between the two coil supports substantially corresponds to that part of the area of the pole gap in the radial direction which is not occupied by a coil support. Through this is ascertained that the area available for the flow of cooling gas in the axial direction, between each support in a pair, is substantially equal to the area available in the radial direction, i.e. that area in a pole gap where the air flow is not prevented by a pole support.

Rotating electric machines have conventionally been designed for voltages in the range 6-30 kV, and 30 kV has normally been considered to be an upper limit. This generally means that a generator must be connected to the power network via  
5 a transformer which steps up the voltage to the level of the power network, i.e. in the range of approximately 130-400 kV.

By using high-voltage insulated electric conductors, also  
10 termed high-voltage cables, with solid insulation similar to that used in cables for transmitting electric power (e.g. XLPE cables) the voltage of the machine can be increased to such levels that it can be connected directly to the power network without an intermediate transformer. The conven-  
15 tional transformer can thus be eliminated. However, an important condition for this is that satisfactory ventilation can be arranged, which is thus enabled by the present invention.

20 The present invention is in the first place intended for use with high voltages. High voltages shall be understood here to mean electric voltages in excess of 10 kV. A typical operating range for a device according to the invention may be voltages from 36 kV up to 800 kV. In the second place the  
25 invention is intended for use in the stated technical area at voltages below 36 kV.

For a better understanding of the invention an embodiment will now be described by way of example, with reference to  
30 the accompanying drawings in which:

Figure 1 shows schematically a rotating electric machine from the side, partially in section,

Figure 2a shows a detailed view of a coil support, seen from  
35 above,

Figure 3 shows a detailed view of another coil support, seen from above, and

Figure 4 shows a cross section through a high-voltage cable.

5 A rotating electric machine according to the present invention, seen from the side and partially in cross section, is shown in Figure 1. The machine comprises a rotor 1 with a central axis 2, and a stator 4 provided with windings, preferably composed of high-voltage cable 3, drawn through slots in the stator. The rotor 1 is provided, in a known  
10 manner, with poles, 5, 6, see Figures 2 and 3. The poles comprise pole pieces 8, 9, each provided with windings 10, 11 to form solenoids. Between the poles, provided with the windings, is a space termed the pole gap 13. There is thus a pole gap between each pair of poles and these pole gaps  
15 extend axially along the entire poles, parallel with the central axis of the rotor.

Coil supports 15, 16 are arranged in the pole gaps in order to keep the solenoid windings 10, 11 in place. The coil  
20 supports in the embodiment shown are designed to work in pairs. Each coil support thus supports a part of the windings on the poles adjacent to the pole gap where the relevant coil support is applied.

25 The coil support 15 in Figure 2 is a body in the form of a wedge with truncated tip, its sides abutting the coil windings. The coil support fills approximately half of the area in radial direction, which the pole gap occupies of the space between the windings. The coil support in Figure 2 is  
30 arranged to support those windings, of the respective adjacent poles, which are furthest away from the central axis of the rotor.

The coil support in Figure 3, however, is arranged to support those windings, of the respective adjacent poles, which  
35 are nearest to the central axis of the rotor. In this case also, the coil support is in the form of a wedge-shaped

body, the point being only slightly truncated, or possibly not at all. The sides of the body are in contact with and support the windings. Here, also, the body occupies approximately half the area available in the pole gap in the radial direction between the windings.

Since it is desirable for the air flow between and past the coil supports to be as uniform as possible, it is desirable for the area available to the air flow to be approximately the same size, regardless of whether the coil support is situated and designed as in Figure 2 or as in Figure 3. The coil supports in the two figures ought to occupy approximately equal areas. However, more exact dimensioning of each coil support is controlled in the first place by a striving towards the coil bolts 21 and 22 for the coil supports 15 and 16 taking up an equal load. The two coil supports in a pair according to the invention do not necessarily support the same number of winding turns each. Since, furthermore, for reasons of safety it is suitable for the coil supports working in pairs to be able to support the windings in the boundary area between two coil supports with a certain amount of overlap, since a certain amount of difficulty may be encountered in placing out the coil supports perfectly exactly, the coil support according to the embodiment in Figure 3 will preferably support a few more than half of the windings, whereas the coil support in Figure 2 supports approximately half of the windings.

Both the coil supports 15, 16 are provided with means for attachment to the rotor. In the example illustrated the coil supports are provided with a central boring 19, 20, through which an attachment screw/support bolt 21, 22 or the like can be applied. The rotor is provided with a corresponding boring so that the attachment screw can be passed through the coil support and secured in the rotor.

Reference is again made to Figure 1 revealing how ventilation and cooling of the poles, etc. is achieved. The path of the cooling air is indicated by arrows 23. The machine includes a fan 24, which conveys cooling air axially from above into the available space, i.e. the pole gaps between the poles. The air is transported by means of this fan from the upper side of the rotor to the lower side. The air flows between the coil supports, thereby cooling the windings, and continues downwards towards the lower side of the stator where the complete lower coil-end package 25 is cooled by the same air. The air can then continue up and out through the stator 4 in order to cool this.

Finally, Figure 4 shows a cross section through a high-voltage cable 3, which is particularly suitable for use with the present invention. The high-voltage cable 3 is composed of a number of strand parts 31 made of copper (Cu), for instance, and having circular cross section. These strand parts are arranged in the middle of the high-voltage cable. Surrounding the strand parts 31 is a first semiconducting layer 32. Surrounding the first semiconducting layer 32 is an insulating layer 33, e.g. XLPE-insulation, and surrounding the insulating layer 33 is a second semiconducting layer 34. The cable illustrated differs from conventional high-voltage cable in that the outer, mechanically protective sheath and the metal screen that normally surround such a cable have been eliminated. The concept "high-voltage cable" in the present application thus need not include the metal screen and the outer protective sheath that normally surround such a cable for power distribution.

In the embodiment illustrated, the two coil supports could be compared with dividing a conventional coil support into two parts, each of which is radially smaller and which are arranged at radially different distances from the central axis of the rotor. However, the invention shall not be deemed limited to this embodiment but can be varied within

the scope of the inventive concept as defined in the appended claims, e.g. by different shape and/or dimensioning of the coil supports in relation to each other, or by providing the coil supports with apertures in a suitable manner, in order to further increase the area available for the flow of cooling air.

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## CLAIMS

1. A rotating electric machine comprising a stator (4) provided with windings inserted in slots in the stator, and  
5 a rotor (1) having a central axis (2) and poles (5, 6) in the form of pole pieces (8, 9) provided with windings and forming solenoids, in which rotor pole gaps (13) are being provided between the poles, and comprising coil supports (15, 16) disposed in said pole gaps in order to support the  
10 solenoid windings (10, 11), characterized in that the coil supports (15, 16) are arranged in pairs, that each of said coil supports (15, 16) in a pair is shaped so that it supports only a part of the solenoid windings (10, 11) of the two adjacent poles (5, 6), and that two coil supports  
15 (15, 16) in a pair are arranged axially and radially displaced in relation to each other to allow a cooling gas to flow between the coil supports.

2. A rotating electric machine as claimed in claim 1,  
20 characterized in that the winding is flexible and comprising an electrically conducting core surrounded by an inner semiconducting layer (32), an insulating layer (33) surrounding the inner semiconducting layer and consisting of solid material, and an outer semiconducting layer (34)  
25 surrounding the insulating layer, said layers adhering to each other.

3. A rotating electric machine as claimed in claim 2,  
characterized in that said layers (32, 33, 34)  
30 consist of materials having such elasticity and with such a relation between the coefficients of thermal expansion of the materials that the changes in volume in the layers caused by temperature fluctuations during operation can be absorbed by the elasticity of the materials, the layers thus  
35 retaining their adhesion to each other upon the temperature fluctuations that occur during operation.

4. A rotating electric machine as claimed in claim 3,  
characterized in that the materials in said layers  
(32, 33, 34) have high elasticity, preferably with an E-  
modulus less than 500 MPa, most preferably less than  
5 200 MPa.

5. A rotating electric machine as claimed in claim 3,  
characterized in that the coefficients of thermal  
expansion for the materials in said layers (32, 33, 34) are  
10 of substantially the same magnitude.

6. A rotating electric machine as claimed in claim 3,  
characterized in that the adhesion between the  
layers (32, 33, 34) is of at least the same magnitude as in  
15 the weakest of the materials.

7. A rotating electric machine as claimed in claim 2 or  
claim 3, characterized in that each of the semicon-  
ducting layers (32, 34) essentially constitutes one equipo-  
20 tential surface.

8. A rotating electric machine as claimed in any of  
claims 2-7, characterized in that the windings of  
the stator (4) consist of high-voltage cable (3).  
25

9. A rotating electric machine as claimed in claim 8,  
characterized in that the high-voltage cable (3)  
has a diameter within the interval 20-250 mm and a conduct-  
ing area within the interval 80-3000 mm<sup>2</sup>.  
30

10. A rotating electric machine as claimed in any of the  
preceding claims, characterized in that each of the  
two coil supports (15, 16) in a pair occupies substantially  
half of the area of the corresponding pole gap (13) in the  
35 radial direction.

11. A rotating electric machine as claimed in any of the preceding claims, characterized in that one of the two coil supports (15, 16) in a pair is arranged to support substantially half of the windings (10, 11) of the two adjacent poles (5, 6) and that the other of the two coil supports is arranged to support substantially the other half of said windings.

12. A rotating electric machine as claimed in any of the preceding claims, characterized in that one of the two coil supports (15, 16) in a pair is arranged to support substantially half of the windings (10, 11) of the two adjacent poles (5, 6) and that the other of the two coil supports is arranged to support the other half of said windings and an additional small number of windings in order to secure an overlap of supported windings.

13. A rotating electric machine as claimed in any one of claims 10, 11 or 12, characterized in that the two coil supports (15, 16) in a pair are displaced axially by such a distance that the area in the axial direction between the two coil supports substantially corresponds to that part of the area of the pole gap (13) in the radial direction which is not occupied by a coil support.

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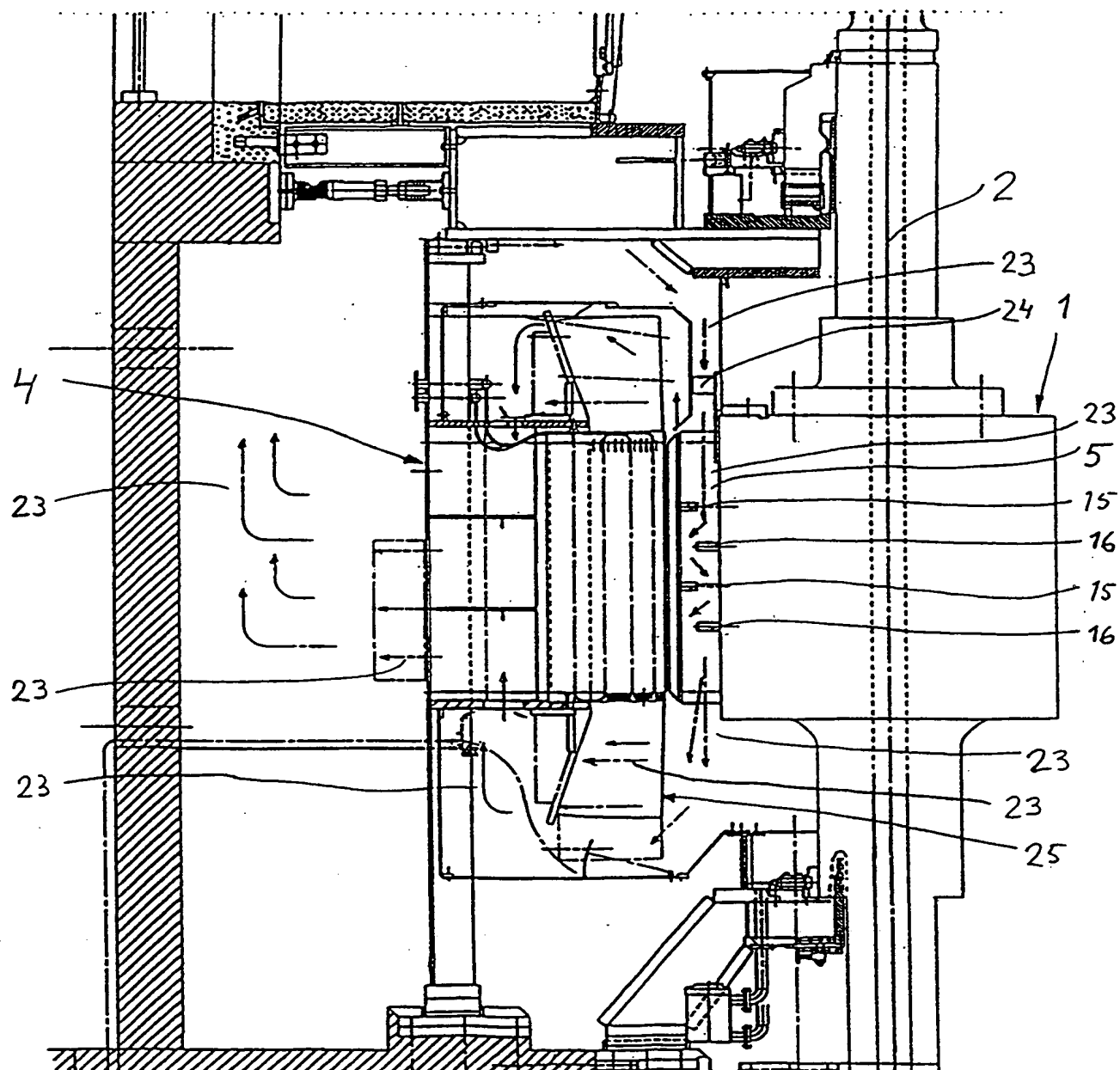


Fig. 1

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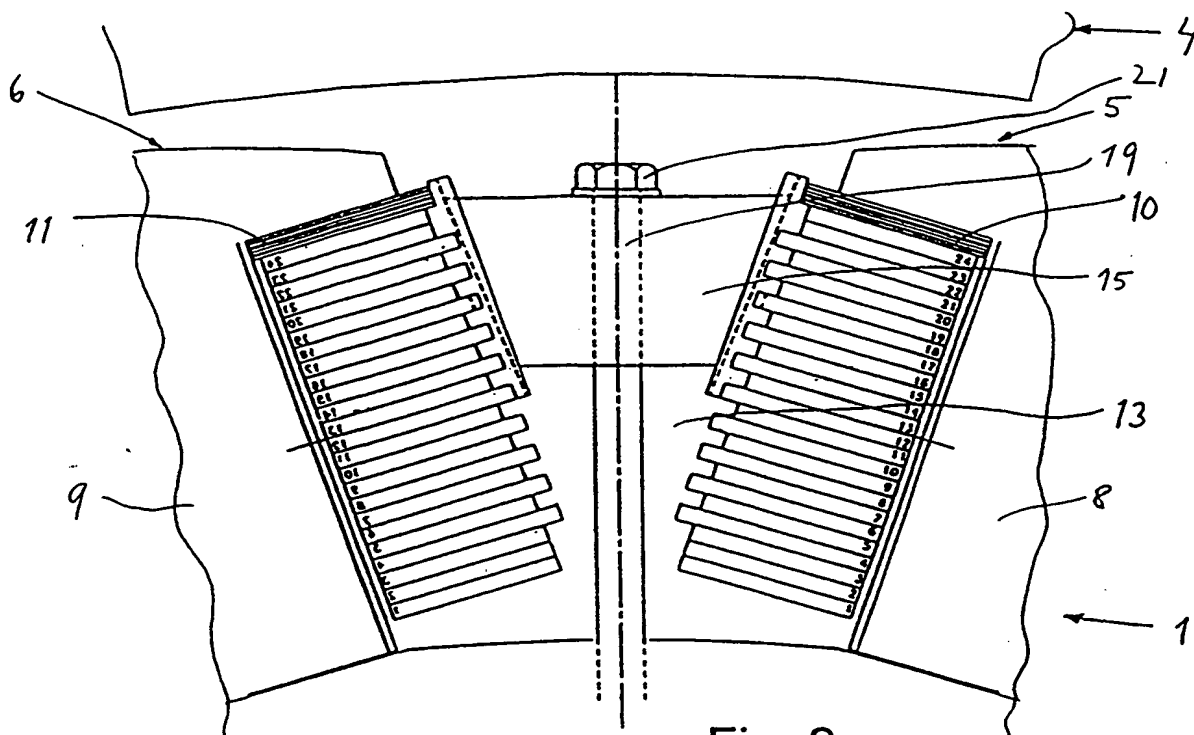


Fig. 2

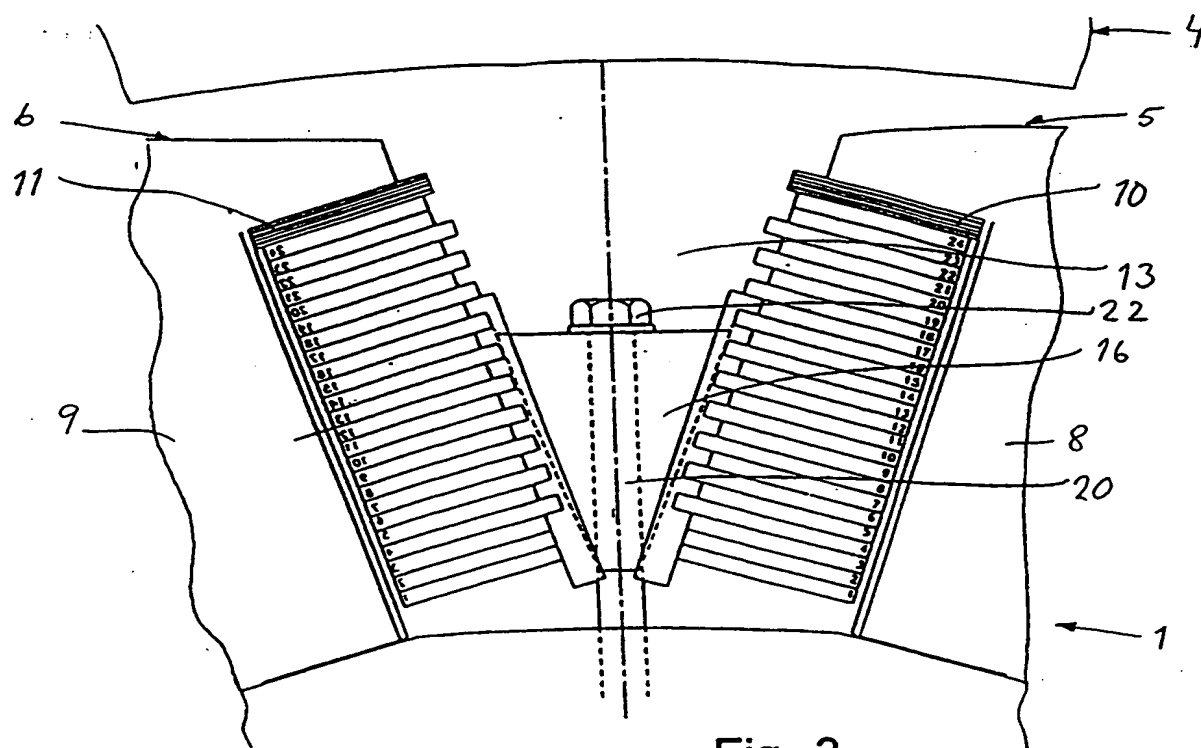


Fig. 3

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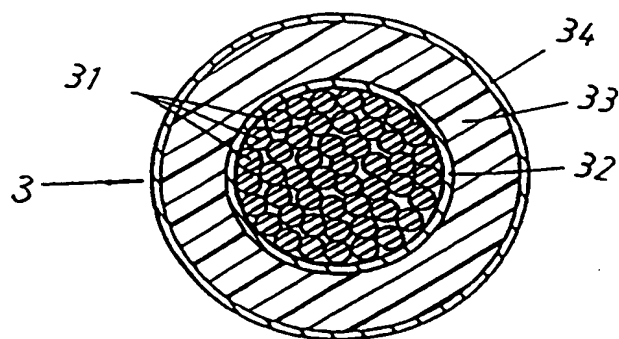


Fig. 4

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# INTERNATIONAL SEARCH REPORT

International application No.  
PCT/SE 98/00164

## A. CLASSIFICATION OF SUBJECT MATTER

IPC6: H02K 3/52

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC6: H02K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPI

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4795933 A (KOICHI SAKAI), 3 January 1989 (03.01.89), column 2, line 67 - column 3, line 37, figure 3 --	1-13
A	DE 2520511 A1 (SIEMENS AG), 18 November 1976 (18.11.76), figure 1 --	1-13
A	GB 2022327 A (BBC BROWN BOVERI & COMPANY LIMITED), 12 December 1979 (12.12.79), figures 1-5 --	1-13
A	US 3740600 A (BARRY J. TURLEY), 19 June 1973 (19.06.73), column 4, line 19 - line 22, figure 2, abstract --	1-13

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

\* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
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- "P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"&" document member of the same patent family

Date of the actual completion of the international search

6 July 1998

Date of mailing of the international search report

07 -07- 1998

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# INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 98/00164

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5036238 A (MASAAKI TAJIMA), 30 July 1991 (30.07.91), figures 1,2  --	1-13
A	US 5036165 A (RICHARD K. ELTON ET AL), 30 July 1991 (30.07.91), column 1, line 22 - line 50, figure 1  -- -----	2-9

# INTERNATIONAL SEARCH REPORT

Information on patent family members

30/06/98

International application No.

PCT/SE 98/00164

Patent document cited in search report			Publication date	Patent family member(s)		Publication date
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